

# **AFFECTED SYSTEM STUDY** TSR 90918528

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By SPP Engineering, Transmission Services

# **REVISION HISTORY**

DATE OR VERSION NUMBER	AUTHOR	CHANGE DESCRIPTION	COMMENTS
07/02/2020	SPP	Original	

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### **EXECUTIVE SUMMARY**

Associated Electric Cooperative, Inc (AECI) received a 1,000 MW TSR request from AECI to MISO.S. In accordance with the JOA they notified SPP of this TSR so that SPP could study the request to determine if there were any impacts on the SPP system. The period of the service requested is from 1/1/2025 to 1/1/2030.

The principal objective of this study is to identify system problems and potential system modifications necessary to facilitate the TSR request while maintaining system reliability. SPP studied this request using the base reliability scenarios of the 2020 ITP model series.

The service caused one SPP branch to overload and several first-tier entity facilities to overload.

### **INTRODUCTION**

This study includes steady-state contingency analysis (Power System Simulator for Engineering (PSS/E) function ACCC). The steady-state analysis considers the impact of the request on transmission line and transformer loadings, and bus voltages for outages of single transmission lines, transformers, and generating units, and selected multiple transmission lines and transformers on the SPP and third party systems.

SPP studied the request by using modified Base Reliability models to reflect the current modeling information. Base Reliability includes projected usage of transmission included in the SPP 2020 ITP Cases.

### STUDY METHODOLOGY

### DESCRIPTION

SPP conducted the facility study analysis to determine the steady-state impact of the requested service on the SPP and first-tier non-SPP control area systems. SPP performed the steady-state analysis that was consistent with current SPP Criteria and North American Electric Reliability Corporation (NERC) Reliability Standards requirements. SPP conforms to NERC Reliability Standards, which provide strict requirements related to voltage violations and thermal overloads during normal conditions and during a contingency. NERC Standards require all facilities to be within normal operating ratings for normal system conditions and within emergency ratings after a contingency.

Normal operating ratings and emergency operating ratings monitored are Rate A and B in the SPP Integrated Transmission Planning (ITP) models, respectively. The upper bound and lower bound of the normal voltage range monitored is 105% and 95%. The upper bound and lower bound of the emergency voltage range monitored is 105% and 90%.

The contingency set includes all SPP control area branches and ties 69 kV and above; first-tier non-SPP control area branches and ties 115 kV and above; any defined contingencies for these control areas; and generation unit outages for the control areas with SPP reserve share program redispatch. The monitored elements include all SPP control area branches, ties, and buses 69 kV and above, and all first-tier non-SPP control area branches and ties 115 kV and above. SPP performs voltage monitoring for SPP control area buses 69 kV and above.

SPP applied the appropriate TDF cutoffs (SPP and third party) to determine the impacted facilities.

### MODEL DEVELOPMENT

SPP used the following 2020 ITP models, used in the 2020 ITP Assessment, to study the impact of the requested service on the transmission system:

- 2025 Light Load, Summer, and Winter
- 2030 Light Load, Summer, and Winter

The Summer Peak models apply to June through September and the Winter Peak models apply to December through March. The Light Load models apply to April through May.

The chosen base case models were modified to reflect the current modeling information, including confirmed transactions from previous studies. Base Reliability scenarios include projected usage of transmission included in the SPP 2020 ITP Cases.

### TRANSMISSION REQUEST MODELING

SPP modeled the request as a generation-to-generation transfer. TDFs were computed based on generation-to-generation and generation-to-load configurations.

#### TRANSFER ANALYSIS

SPP compared the results (with and without the requested transfer modeled) by using the PSS/E Activity ACCC to determine the facility overloads caused by the transfer. In addition, SPP applied the appropriate TDF cutoffs (SPP and third party) to determine the impacted facilities. Appendix A lists the PSS/E options chosen to conduct the analysis.

### STUDY RESULTS

### SPP STUDY ANALYSIS RESULTS

Table 1 lists SPP thermal transfer limitations caused by the transfer.

Season	Area	Monitored Branch	Base Case Loading (%)	Transfer Case Loading (%)	Contingency
25SP	KCPL	SALSBRY5-NORTON 5 161kV	64.2	101.2	P12:345:AMMO::MONTGOMERY:OVERTON:5
25SP	KCPL	SALSBRY5-NORTON 5 161kV	63.9	101.0	P23:345:AMMO::MONTGOMERY:V43
30SP	KCPL	SALSBRY5-NORTON 5 161kV	68.8	105.8	P12:345:AMMO::MONTGOMERY:OVERTON:5
30SP	KCPL	SALSBRY5-NORTON 5 161kV	68.6	105.6	P23:345:AMMO::MONTGOMERY:V43

Table 1: SPP Thermal Violations

Table 2 details the SPP-assigned network upgrades required to implement the 1,000 MW transmission service request.

#### Table 2: SPP Assigned Network Upgrade

Upgrade Description	Cost Estimate	Est. In-Service
Salisbury – Norton 161kV terminal upgrades	\$125,000	January, 2023

### THIRD PARTY STUDY ANALYSIS RESULTS

Table 3 lists third party thermal transfer limitations caused by the transfer.

Season	Area	Monitored Branch	Base Case Loading (%)	Transfer Case Loading (%)	Contingency
25SP	AECI	MLRSBGB1-5BOONE 161kV	49.2	136.4	P12:345:AMMO::MONTGOMERY:OVERTON:5
25SP	AECI	MLRSBGB1-5BOONE 161kV	48.9	136.1	P23:345:AMMO::MONTGOMERY:V43
25WP	AECI	MLRSBGB1-5BOONE 161kV	41.9	123.8	P12:345:AMMO::MONTGOMERY:OVERTON:5
25WP	AECI	MLRSBGB1-5BOONE 161kV	41.5	123.5	P23:345:AMMO::MONTGOMERY:V43
30SP	AECI	MLRSBGB1-5BOONE 161kV	52.5	139.7	P12:345:AMMO::MONTGOMERY:OVERTON:5
30SP	AECI	MLRSBGB1-5BOONE 161kV	52.1	139.3	P23:345:AMMO::MONTGOMERY:V43
30WP	AECI	MLRSBGB1-5BOONE 161kV	42.2	124.3	P12:345:AMMO::MONTGOMERY:OVERTON:5
30WP	AECI	MLRSBGB1-5BOONE 161kV	41.8	123.8	P23:345:AMMO::MONTGOMERY:V43
25SP	AECI	5KINGDMB1-5MLRSBGB2 161kV	52.8	140.0	P12:345:AMMO::MONTGOMERY:OVERTON:5
25SP	AECI	5KINGDMB1-5MLRSBGB2 161kV	52.4	139.7	P23:345:AMMO::MONTGOMERY:V43

Season	Area	Monitored Branch	Base Case Loading (%)	Transfer Case Loading (%)	Contingency
25WP	AECI	5KINGDMB1-5MLRSBGB2 161kV	39.8	111.0	P12:345:AMMO::MONTGOMERY:OVERTON:5
25WP	AECI	5KINGDMB1-5MLRSBGB2 161kV	39.4	110.7	P23:345:AMMO::MONTGOMERY:V43
30SP	AECI	5KINGDMB1-5MLRSBGB2 161kV	56.3	143.6	P12:345:AMMO::MONTGOMERY:OVERTON:5
30SP	AECI	5KINGDMB1-5MLRSBGB2 161kV	55.9	143.2	P23:345:AMMO::MONTGOMERY:V43
30WP	AECI	5KINGDMB1-5MLRSBGB2 161kV	40.2	111.6	P12:345:AMMO::MONTGOMERY:OVERTON:5
30WP	AECI	5KINGDMB1-5MLRSBGB2 161kV	39.8	111.1	P23:345:AMMO::MONTGOMERY:V43
25SP	AECI	5THMHILB1-5MOBTAP 161kV	65.9	102.0	P12:345:AMMO::MONTGOMERY:OVERTON:5
25SP	AECI	5THMHILB1-5MOBTAP 161kV	65.7	101.9	P23:345:AMMO::MONTGOMERY:V43
25WP	AECI	5THMHILB1-5MOBTAP 161kV	68.5	105.6	P12:345:AMMO::MONTGOMERY:OVERTON:5
25WP	AECI	5THMHILB1-5MOBTAP 161kV	68.3	105.4	P23:345:AMMO::MONTGOMERY:V43
30SP	AECI	5THMHILB1-5MOBTAP 161kV	69.1	105.4	P12:345:AMMO::MONTGOMERY:OVERTON:5
30SP	AECI	5THMHILB1-5MOBTAP 161kV	69.0	105.3	P23:345:AMMO::MONTGOMERY:V43
30WP	AECI	5THMHILB1-5MOBTAP 161kV	69.0	106.0	P12:345:AMMO::MONTGOMERY:OVERTON:5
30WP	AECI	5THMHILB1-5MOBTAP 161kV	68.8	105.7	P23:345:AMMO::MONTGOMERY:V43
25SP	AECI	5THOMHLXF3-5THMHLB3 161kV	83.5	103.2	7THOMHL - 5THOMHLXF4 - 4
25SP	AECI	5THOMHLXF3-5THMHLB3 161kV	83.5	103.0	5THMHLB4 - 5THOMHLXF4 - 1
25SP	AECI	5THOMHLXF3-5THMHLB3 161kV	49.4	102.5	P12:345:AMMO::MONTGOMERY:OVERTON:5
30SP	AECI	5THOMHLXF3-5THMHLB3 161kV	83.1	102.4	5THMHLB4 - 5THOMHLXF4 - 1
30SP	AECI	5THOMHLXF3-5THMHLB3 161kV	49.1	102.3	P12:345:AMMO::MONTGOMERY:OVERTON:5
25SP	AECI	7KINGDM-5KINGDMB1 345/161kV	36.8	127.9	P23:345:AMMO::MONTGOMERY:V43
25WP	AECI	7KINGDM-5KINGDMB1 345/161kV	42.8	122.0	P23:345:AMMO::MONTGOMERY:V43
30LP	AECI	7KINGDM-5KINGDMB1 345/161kV	13.5	100.2	P12:345:AMMO::MONTGOMERY:OVERTON:5
30LP	AECI	7KINGDM-5KINGDMB1 345/161kV	13.5	100.1	P23:345:AMMO::MONTGOMERY:V43
30SP	AECI	7KINGDM-5KINGDMB1 345/161kV	37.6	128.7	P12:345:AMMO::MONTGOMERY:OVERTON:5
30WP	AECI	7KINGDM-5KINGDMB1 345/161kV	42.4	121.6	P12:345:AMMO::MONTGOMERY:OVERTON:5
30WP	AECI	7KINGDM-5KINGDMB1 345/161kV	42.4	121.5	P23:345:AMMO::MONTGOMERY:V43
25SP	AECI	7THOMHL-5THOMHLXF4 345/161kV	91.0	112.2	7THOMHL - 5THOMHLXF3 - 3
30SP	AECI	7THOMHL-5THOMHLXF4 345/161kV	90.6	111.5	7THOMHL - 5THOMHLXF3 - 3
25LP	AMMO	4JOACHIM 2-4BOYD BR 138kV	91.1	104.4	P23:345:AMMO::STFRANCOIS:V15
30LP	AMMO	4JOACHIM 2-4BOYD BR 138kV	87.8	101.0	P23:345:AMMO::STFRANCOIS:V15
25SP	EES	6ADMSCRK%-6BOGALUS% 230kV	96.7	100.9	6ADMSCRK% - 6BOGALUS% - 2
25SP	EES	6ADMSCRK%-6BOGALUS% 230kV	96.7	100.9	6ADMSCRK% - 6BOGALUS% - 1

# CONCLUSION

Associated Electric Cooperative, Inc (AECI) received a 1,000 MW TSR request from AECI to MISO.S. In accordance with the JOA they notified SPP of this TSR so that SPP could study the request to determine if there were any impacts on the SPP system. The period of the service requested is from 1/1/2025 to 1/1/2030.

SPP has conducted an affected system study to determine if there are any impacts to the SPP system based on this request. The analysis has determined that an SPP assigned network upgrade will be required as listed in Table 2.

## APPENDIX A

#### PSS/E OPTIONS IN RUNNING LOAD FLOW PROGRAM AND ACCC

#### BASE CASE SETTINGS:

- Solutions:
- Tap adjustment:
- Area Interchange Control:
- VAR limits:
- Solution Options:

Fixed slope decoupled Newton-Raphson solution (FDNS) Stepping Tie lines and loads Apply immediately

<u>X</u> Phase shift adjustment \_\_ Flat start \_\_ Lock DC taps

#### \_ Lock switched shunts

### ACCC CASE SETTINGS:

- Solutions:
- MW mismatch tolerance:
- System intact rating:
- Contingency case rating:
- Percent of rating:
- Output code:
- Minimum flow change in overload report:
- Exclude cases w/ no overloads from report:
- Exclude interfaces from report:
- Perform voltage limit check:
- Elements in available capacity table:
- Cutoff threshold for available capacity table:
- Minimum contingency case voltage change for report:
- Sorted output:
- Newton Solution:
- Tap adjustment:
- Area Interchange Control:
- VAR limits:
- Solution options:

AC contingency checking (ACCC) 0.5 Rate A Rate B 100 Summary 3 MW YES No Yes 60,000 99,999 0.02 None Stepping Tie lines and loads (Disabled for generator outages) Apply immediately X Phase shift adjustment \_ Flat start

- \_ Lock DC taps
- \_ Lock switched shunts